COPYRIGHT[©] INTERNATIONAL ISLAMIC UNIVERSITY MALAYSIA

DEVELOPMENT OF MATHEMATICAL MODELS AND ONLINE CHATTER CONTROL SYSTEM IN TURNING AISI 304 STAINLESS STEEL

BY

MUAMMER DIN ARIF

A thesis submitted in fulfilment of the requirement for the degree of Doctor of Philosophy (Engineering)

Kulliyyah of Engineering International Islamic University Malaysia

AUGUST 2019

ABSTRACT

Chatter is intensive self-excited vibration of the individual components of a Machine-Tool-Fixture-Work (MTFW) system which reduces tool life, accuracy, surface finish quality and productivity. In turning, it manifests itself as bouncing in and out of the tool shank from the flexible work-piece. However, it is a complex process and so no comprehensive theory has yet been developed. Thus, research into the root cause of chatter, its formation mechanism, mathematical modelling and chatter suppression is very important to industry and academia. The prevalent theories on chatter are controversial; often contradicted by experimental evidences. The Regeneration Theory posits that surface waviness left from a previous cut interferes with the next machining pass and leads to chatter. In contrast, the Resonance Theory states that chatter occurs due to resonance when the chip serration frequency coincides with the natural frequencies of the MTFW system. The current research investigated chip serration frequency, cutting force, mode shapes and natural frequencies of the tool shank, and vibration amplitudes during turning of AISI 304 stainless steel under different combinations of primary cutting parameters with the aim to model the responses and gain understanding of chatter. The work material, AISI 304 stainless steel, was turned on an engine lathe using TiN-coated cemented carbide inserts. Small Central Composite Design (CCD) modelling approach in Response Surface Methodology (RSM) was used for designed experiments and resulted in quadratic empirical mathematical models of vibration amplitude and chip serration frequency, and two-factor interaction (2FI) model for cutting force; which were subsequently analysed by ANOVA. It was found that, cutting speed (V_c) and depth of cut (DOC) had quadratic perturbation effect in determining the responses. Next, the postulates of the Resonance Theory of Chatter and energy balance method were used to analytically explain chatter as the consequence of P_{max} (vibration energy) at the resonance of tool shank's mode shapes. It was found that chatter occurred when chip serrations approached even integer multiples of the two dominant resonant frequencies (transverse and torsional) of the tool shank ($f_c = 10f_{n1}$, $20f_{n1}$, $30f_{n1}$ and $f_c = 2f_{n5}$, $4f_{n5}$, $6f_{n5}$) due to mode coupling; resulting in large peak values of cutting force and chatter. The empirical models were numerically and graphically optimised and showed that chatter was more prone to occur for combinations of high cutting speed (near 200 m/min) and large depths of cuts (2 mm or more). Concurrently, an electromagnetbased online chatter control system was developed which was controlled by a closedloop feedback proportional and integral (PI) controller developed in LabVIEW. This controller detected and minimised chatter amplitude by 46% (on average); treating it as a disturbance in the turning process. The damping was provided by the uniform magnetic field produced by the electromagnet which resisted any movement of the ferromagnetic steel tool shank. This active damper is economical and robust; capable of handling all conditions of cut of the CCD model. Hence, this research developed an in-depth understanding of chatter, modelled it using empirical, statistical and analytical methods which were able to predict stable cutting regions. An economical and effective online chatter control system was successfully developed.

لاصة البحث

الذبذبة هي عبارة عن اهتزاز ذاتي مكثف للمكونات الفردية لنظام (MTFW). و تقوم هذه الذبذبة بالتَّقليل من عمر الأداة و دفتَّها و جودة السطح النهائية و انتاجيتها. اثناء الدوران تظهر الذبذبة كارتداد داخل و خارج ذراع الأداة من مرونة قطعة العمل. و مع ذلك فهي تعتبر عملية معقدة و بالتالي لم يتم تطوير أي نظرية شاملة. إن البحث في الأسباب الجذرية للذبذبة و آلية تشكيلها و تصميمها الرياضي و إيقاف هذه الذبذبة لهو أمر مهم جدا للصناعة و للوسط الأكاديمي. النظريات السائدة في الذبذبة مثيرة للجدل و غالبًا ما تتناقض مع الأدلة التجريبية. تفترض نظرية التجديد أن التباين السطحي المتبقى من قطع سابق يتداخل مع القطع التالي مما يؤدي إلى الذبذبة. في المقابل تنص نظرية الرنين على أن الذبذبة تحدث بسبب الرنين عندما يتزامن تردد القصاصة مع الترددات الطبيعية لنظام (MTFW). قام الطالب من خلال هذه الدراسة بالتحقيق عن تردد رقاقة الرنين , و قوة القطع , و اشكال الوضع , و الترددات الطبيعية من ذراع الأداة , و سعة الاهتزاز أثناء تحويل AISI 304 (الفولاذ المقاوم للصدأ) تحت مجاميع مختلفة من عوامل القطع الأولية لهدف خلق نموذج للاستجابات لغرض فهم عملية الذبذبة. تم تشغيل مادة AISI 304 (الفولاذ المقاوم للصدأ) على مخرطة محرك باستخدام رؤوس قطع مغلفة ب cemented TiN من الكربيد. وقد تم استخدام منهج التصميم المركب المركزي (CCD) في منهجية الاستجابة السطحية (RSM) للتجارب المصممة , و أسفرت عن نماذج حسابية تجريبية تربيعية لسعة الاهتزاز و تردد رقاقة الرنين , و نموذجين للتفاعل (2FI) لقوة القطع التي تم تحليلها لاحقا باستخدام ANOVA. وجد بأن سرعة القطع (V_c) و عمق القطع (DOC) له تأثير اضطراب تربيعي في تحديد الاستجابات. بعد ذلك تم استخدام فرضيات نظرية الرنين من الذبذبة و طريقة توازن الطاقة لتفسير الذبذبة كنتيجة ل P_{max} (طاقة الاهتزاز) عند رنين اشكال الوضع لذراع الأداة. و قد وجد أيضا أن الذبذبة تحدث نتيجة اقتراب رقاقات القطع من مضاعفات عدد صحيح من ترددات الرنين (المستعرضة و الالتوائية) لذراع الاداة (fc =) بسبب اقتران الوضع مما أدى إلى قيم ذروة ($10f_{n1}, 20f_{n1}, 30f_{n1}$ and $f_c = 2f_{n5}, 4f_{n5}, 6f_{n5}$ كبيرة من قوة القطع و الذبذبة. كانت النماذج التجريبية محسنة من الناحية العددية والرسومات البيانية , وأظهرت أن الذبذبة كانت أكثر عرضة لمجاميع قطع عالية السرعة (قرب 200 م / دقيقة) و قطع عميقة (2 مليمتر أو أكثر). و في الوقت نفسه تم تطوير نظام للتحكم في الذبذبة و يتم التحكم فيه عن طريق جهاز تحكم (PI) المطور في LabVIEW. قام هذا الجهاز باكتشاف وخفض نسبة سعة الذبذبة الى % 46 (في المتوسط) و تم التعامل معها على انها اضطراب في عملية الدوران. و قد تم تزويد اداة لتخميد الذبذبة عن طريق الحقل المغناطيسي الموحد الناتج عن المغناطيس الكهربائي و الذي يقوم بمقاومة اي حركة من الأداة الحديدية المغناطيسية. اداة التخميد هذة تتسمبالاقتصادية و القوة , و هو قادر على التعامل مع جميع حالات القطع لنموذج ال CCD. فمن خلال هذا البحث حصلنا على فهم موسع للذبذبة باستخدام أساليب تجريبية و إحصائية و تحليلية , و قمنا بالتنبؤ بالمناطق المستقرة للقطع , و أخيرا تمكنا من تطوير نظام تحكم جاهز بالذبذبة

APPROVAL PAGE

The thesis of Muammer Din Arif has been approved by the following:

Mohamed Bin Abd Rahman Supervisor

Mohammad Yeakub Ali Co-Supervisor

Muataz Hazza Faizi Al Hazza Co-Supervisor

> A. K. M. Nurul Amin Field Supervisor

Erry Yulian Triblas Adesta Internal Examiner

Imtiaz Ahmed Choudhury External Examiner

> Yusri Yusof External Examiner

> > Rafikul Islam Chairman

DECLARATION

I hereby declare that this thesis is the result of my own investigations, except where otherwise stated. I also declare that it has not been previously or concurrently submitted as a whole for any other degrees at IIUM or other institutions.

Muammer Din Arif

Signature

Date

INTERNATIONAL ISLAMIC UNIVERSITY MALAYSIA

DECLARATION OF COPYRIGHT AND AFFIRMATION OF FAIR USE OF UNPUBLISHED RESEARCH

DEVELOPMENT OF MATHEMATICAL MODELS AND ONLINE CHATTER CONTROL SYSTEM IN TURNING AISI 304 STAINLESS STEEL

I declare that the copyright holders of this thesis are jointly owned by the student and IIUM.

Copyright © 2019 Muammer Din Arif and International Islamic University Malaysia. All rights reserved.

No part of this unpublished research may be reproduced, stored in a retrieval system, or transmitted, in any form or by any means, electronic, mechanical, photocopying, recording or otherwise without prior written permission of the copyright holder except as provided below

- 1. Any material contained in or derived from this unpublished research may be used by others in their writing with due acknowledgement.
- 2. IIUM or its library will have the right to make and transmit copies (print or electronic) for institutional and academic purposes.
- 3. The IIUM library will have the right to make, store in a retrieved system and supply copies of this unpublished research if requested by other universities and research libraries.

By signing this form, I acknowledged that I have read and understand the IIUM Intellectual Property Right and Commercialization policy.

Affirmed by Muammer Din Arif

Signature

Date

vi

ACKNOWLEDGEMENTS

Firstly, I wish to express my thankfulness and gratitude to the Almighty for granting me the opportunity and ability to complete my research work and finish the doctoral thesis.

Secondly, I wish to express my sincere gratitude to my thesis supervisor, Associate Professor Dr. Mohamed Bin Abd Rahman for helping, advising and supporting me in pursuing my PhD degree and overcoming many hurdles and obstacles.

Thirdly, I would like to thank the other members of my dissertation committee: Professor Dr. Mohammad Yeakub Ali (Co-Supervisor) and Assistant Professor Dr. Muataz Hazza Faizi Al Hazza (Co-Supervisor). They have guided me to accomplish my goal.

I wish also to express my appreciation and thanks to those who provided their time, effort and support for this project, including esteemed faculty members Assistant Professor Dr. Israd Hakim Bin Jaafar, Associate Professor Dr. Asan Gani Bin Abdul Muthalif, Assistant Professor Dr. Fadly Jashi Darsivan Bin Ridhuan Siradj, Associate Professor Dr. Iskandar Al-Thani Bin Mahmood, Professor Dr. Md. Raisuddin Khan and Associate Professor Dr. Muhammad Mahbubur Rashid. I am also grateful for the help provided by staff members Br. Ibrahim Bin Razali Maarof, Br. Zahir Hussain B. Syed Meera and Dr. Zakaria Bin Mohd. Zain. In addition, I would like to thank my fellow students of the Manufacturing and Materials Engineering Department who supported me in my research work.

Finally, a special thanks to Professor Dr. A.K.M. Nurul Amin (Field Supervisor) for his continuous support, encouragement and leadership throughout my PhD tenure.

In the end, it is my utmost pleasure to dedicate this work to my dear parents, my grandmother, my wife and my little angel Innaya, who granted me the gift of their unwavering belief in my ability, and both financial and mental support to accomplish this goal. Thank you all for your love and patience.

TABLE OF CONTENTS

Abstractii
Abstract in Arabiciii
Approval Pageiv
Declaration
Copyright Pagevi
Acknowledgementsvii
Table of Contents
List of Tablesxii
List of Figuresxiv
List of Abbreviationsxviii
CHAPTER ONE: INTRODUCTION1
1.1 Background1
1.2 Problem Statement
1.3 Significance and Benefits of the Research
1.4 Research Philosophy6
1.5 Scope of the Research7
1.6 Objectives of the Research9
1.7 Research Methodology10
1.8 Thesis Organization
CHAPIER I WU: LIIERAIURE REVIEW
2.1 Introduction15
2.2 Fundamentals of Machining
2.2.1 Chip Formation
2.2.2 Different Types of Vibrations in Machining
2.2.3 Self-Excited Vibrations (Chatter)
2.3 Previous Research Works on Modal Analysis
2.4 The Closed Loop Metal Turning Process and Self-excited Vibrations
(Chatter)
2.5 Cutting Forces in Metal Turning Operations
2.6 Cutting Force Measurement
2.7 Chip Morphology and Serration
2.8 Previous and State-of-the-Art Chatter Research
2.8.1 The Causes of Chatter
2.8.2 Existing Mathematical Models of Chatter
2.9 Chatter Control
2.10 Summary72
CHAPTER THREE: EXPERIMENTAL DETAILS AND

.75
.75
.77
.79
.80

3.2.1.2 Tool Insert	82
3.2.1.3 Work-Piece Material	84
3.2.2 Determination of Natural Frequencies and Mode Shapes of the	
Machine Tool Components	86
3.2.2.1 Finite Element Approach to Modal Analysis	86
3.2.2.2 Experimental Modal Analysis	86
3.2.3 Acquisition and Analysis of Online Vibration Signals	87
3.2.3.1 Sensor	88
3.2.3.2 Signal Processing and Conditioning	89
3.2.4 Analysis of Chip Morphology and Serration	90
3.2.4.1 Scanning Electron Microscope	91
3.2.4.2 Analysis of Saw Teeth Formation	92
3.2.5 Cutting Force Measurement	97
3.2.5.1 Fixture Development for Strain Gauge Calibration	98
3.2.5.2 Dynamometer Calibration	100
3.2.5.3 Acquisition of Online Cutting Force Data	103
3.3 Design of Experiment Using Response Surface Methodology (RSM)	
and Analysis of Data	104
3.3.1 Central Composite Design of RSM	105
3.3.2 Design of Experiment	107
3.3.3 Experimental Design using RSM	107
3.4 Online Chatter Control	108
3.4.1 Design and Development of the Electromagnet and the Fixture	109
3.4.2 Current Controller Details	110
3.4.3 Calibration of the Electromagnet and Current Controller Setup.	111
3.4.4 Graphical Programming in LabVIEW	113
3.4.5 Specification of the PCI Cards	114
3.4.6 Details of the Connector Box	115
3.4.7 Components Setup of the Online Chatter Control	115
3.4.8 Closed-Loop Architecture for Online Chatter Control	
3.4.9 Functional Methodology of the Closed-Loop Controller	
3.5 Summary	120
CHAPTER FOUR. FINITE EI EMENT AND EXPERIMENTAL	
MODAL ANALYSES AND DEVELOPMENT OF EMPIRICAL	
MATHEMATICAL MODELS OF CHATTER	121
4.1 Introduction.	121
4.2 Natural Frequency Determination and Modal Analysis	121
4.2.1 Finite Element Approach to Modal Analysis	121
4.2.2 Experimental Modal Analysis	123
4.3 Experimental Investigation For RSM Model Generation	124
4.4 Mathematical Model for Vibration Amplitude During Turning of	
Stainless Steel	126
4.5 Optimization Using RSM	136
4.5.1 Numerical Optimization	136
4.5.2 Graphical Optimization	138
4.5.3 Experimental Validation of the Model	140
4.6 Mathematical Model for Chip Serration Frequency During Turning	
of Stainless Steel	142

4.7 Mathematical Model for Cutting Force During Turning of Stainless	
Steel	148
4.8 Optimization Using RSM	155
4.8.1 Numerical Optimization	155
4.8.2 Graphical Optimization	157
4.9 Experimental Validation of the Model	159
4.10 Discussion	161
4.11 Summary	163
CHAPTER FIVE: INVESTIGATION OF CHATTER BEHAVIOUR	
WITH CUTTING SPEED VARIATION AND ITS ANALY HCAL	177
EAPLANATION	166 1
5.2 Experimental Investigation of the Influence of Cutting Speed on	100
5.2 Experimental investigation of the influence of Cutting Speed on Vibration Amplitude Cutting Fores and Chin Sometion Frequency	167
vibration Amplitude, Cutting Force and Chip Serration Frequency	10/
5.5 Analytical Mathematical Explanation of Chatter Based on the	170
Resonance Theory of Chatter Formation	1/8
5.3.1 Energy Balance and Single Degree of Freedom Lumped Body	100
Approacn	180
5.4 Discussion	189
5.5 Summary	192
CHADTED SIV. DEVELODMENT AND IMDI EMENTATION OF AN	
ONLINE CHATTER CONTROL SYSTEM	103
6.1 Introduction	193
6.2 Discussion on the Closed-Loop Feedback Control Using PI	175
Controller	194
6 3 Online Chatter Control Details	198
6.3.1 Calibration Runs and PI Tuning	198
6.3.2 Results of Chatter Control Experiments	200
6.3.3 Discussion of the Results	205
6.4 Summary	208
CHAPTER SEVEN: CONCLUSIONS AND RECOMMENDATIONS	
7.1 Conclusions	210
7.2 Major Contributions of the Research	214
7.3 Recommendations for Further Research Studies	215
DEFEDENCES	217
	41 /
RELATED PUBLICATIONS	229
APPENDIX-A VIBRATION GRAPHS (DAMPED AND UNDAMPED)	230
APPENDIX-B RSM RESULTS OF VIBRATION (UNDAMPED TURNING).	
APPENDIX-C CHIP PICTURES FOR RSM RUNS	
APPENDIX-D RSM RESULTS OF CHIP SERRATION	
APPENDIX-E STRAIN GAUGE DYNAMOMETER PICTURES	264
APPENDIX-F RSM RESULTS OF CUTTING FORCE	269
ADDENIDIN O MIDD ATION FOD MADNING CUTTING ODEED	276

APPENDIX-H CHIP PICTURES FOR VARYING CUTTING SPEED	
APPENDIX-I ALL RESULTS OF VARYING CUTTING SPEED	
APPENDIX-J CURRENT CONTROLLER GRAPH	

LIST OF TABLES

Table 2.1 List of Established Research Works Related to Chatter in Machining	45
Table 1.2 Research Works Related to Chatter Control in Machining	66
Table 3.1 Technical Specifications of the Tool Insert in the Research Work	84
Table 3.2 Mechanical Properties of AISI 304 Stainless Steel	85
Table 3.3 Technical Specifications of the Kistler Accelerometer	89
Table 3.4 Details of Dewesoft Software Setup for Vibration Data Acquisition	90
Table 3.5 Results of the Dynamometer Calibration	102
Table 3.6 Experimental Design for CCD Modelling	108
Table 3.7 Technical Specifications of the Electromagnet	109
Table 3.8 Results of the Calibration Experiment Showing Input Current and Resultant Magnetic Force.	113
Table 3.9 List of Critical Components of the Online Chatter Control System	115
Table 4.1 Different Prominent Mode Frequencies of the Tool Shank Determined by FEA Modal Analysis	123
Table 4.2 Experimental Results Obtained for CCD Modelling of Vibration Amplitude	127
Table 4.3 Summary of Statistical Analysis of Vibration Modelling	131
Table 4.4 ANOVA of the Vibration Amplitude Model	132
Table 4.5 Results of the Confirmatory Test with Experimental Validation	142
Table 4.6 Results of the Designed Experiments for Chip Serration Model	144
Table 4.7 ANOVA of the Developed Chip Serration Model	146
Table 4.8 Cutting Force Data for CCD Model	149
Table 4.9 Cutting Force Measurement Comparison with Previous Works	150
Table 4.10 Summary of Statistical Analysis of Cutting Force Model	150
Table 4.11 ANOVA of the Cutting Force Model	151

Table 6.1 Vibration Amplitude Comparison for Undamped and Damped Turning
Involving the 15 DOE Experimental Runs201

160

LIST OF FIGURES

Figure 1.1 Brief Flowchart of the Research Methodology	12
Figure 2.1 The Closed-Loop Process of Chatter: (a) Interaction Between the Machine Tool and the Cutting Process and (b) the Mechanism of Regeneration.	21
	21
Figure 2.2 The Geometry and the Forces involved in Turning Operation	23
Figure 2.3 Micrograph of a Chip in Longitudinal Section During Machining of AISI 1040 Carbon Steel at High Speeds in the Presence of Chatter	27
Figure 3.1 Flow Diagram of Research Methodology for the Development of Mathematical Models of Chatter and Chatter Control Method.	79
Figure 3.2 Schematics of the Experimental Setup	80
Figure 3.3 Picture of the Experimental Setup	80
Figure 3.4 Tool Shank in Turning Operations	82
Figure 3.5 Picture of the TiN Insert.	84
Figure 3.6 Picture of the AISI 304 Stainless Steel Work-piece.	85
Figure 3.7 Picture of the Accelerometer Attached to the Tool Shank	88
Figure 3.8 Picture of the Scanning Electron Microscope	92
Figure 3.9 SEM Images of AISI 304 Stainless Steel Chips Showing: (a) Primary Serrated Teeth and (b) Secondary Serrated Teeth.	93
Figure 3.10 (a) Strain Gauges Glued to Top and Bottom Surfaces of the Tool Shar	ık
and (b) Schematics of the KFG Series General Purpose Kyowa Strain Gauge	98
Figure 3.11 (a) Micro Measurement DAQ Box and (b) Wiring utilized to Acquire Readings from the Strain Gauges and to Feed into the Computer.	98
Figure 3.12 Calibration of Strain Gauge Dynamometer in Universal Testing Machine	99
Figure 3.13 Picture of the Point Load Application Component	100
Figure 3.14 Experimentally Derived Calibration Curve of the Dynamometer	103

Figure 3.15	Experimental Setup Showing: (a) the Strain Gauges Glued to the Tool Shank and (b) the Arrangement for Online Cutting Force Data	
	Acquisition.	103
Figure 3.16	6 Graphical Representation of the Composition of a CCD Model	106
Figure 3.17	Picture of the Electromagnet utilized in Chatter Control Device	109
Figure 3.18	Picture Showing How the Electromagnet was Secured to the Lathe	110
Figure 3.20	Picture of Setup for Calibration of the Electromagnet and Current Controller.	112
Figure 3.21	Force Pull Test Using a Spring Balance and the Electromagnet	112
Figure 3.22	2 Calibration Curve of the Electromagnet and Current Controller Setup	113
Figure 3.23	Arrangements of the Two NI PCI Cards in the Dell Workstation	114
Figure 3.24	A Picture of the NI BNC 2110 Connector Box	115
Figure 3.25	Schematics of the Online Chatter Control System	116
Figure 3.26	6 Pictures of the Online Chatter Control Setup	116
Figure 3.27	Picture of the Block Diagram for Online Chatter Control	118
Figure 3.28	Picture of the Front Panel Showing the Output of 3 Scopes and the Gauge	119
Figure 4.1	Modelling and Analysis of the Tool Shank: (a) 3 D Model Developed Using Catia V, (b) Mesh Generation for Modal Analysis in ANSYS and (c) Determination of the First Eight Fundamental Frequencies.	d 122
Figure 4.2	Mode Shapes of the Tool Shank: (a) $fn1 = 779.66$ Hz, (b) $fn2 = 780.05$ Hz and (c) $fn5 = 4864.1$ Hz.	123
Figure 4.3	FFT Power Spectrum Analysis of Knocking Test for the Tool Shank	124
Figure 4.4	Results of Vibration Analysis for Undamped Turning of Stainless Steel at Cutting Speed 18.93 (m/min), Feed 0.16 (mm/rev) and Depth of Cut (mm) (lowest speed, run 6): (a) is the Time Domain Plot and (b) is the Analysis Showing Peak Vibration Amplitude of 2.92 g at 986.33 Hz.	1.5 FFT 128
Figure 4.5	Vibration Analysis for Undamped Turning of Steel at Cutting Speed 125 (m/min), Feed 0.16 (mm/rev) and DOC 1.5 (mm) (centre run 2): (a Time Domain Plot (b) FFT Analysis Showing Peak Vibration Amplitu at 1025 Hz and 4833 Hz.	a) ides 129
Figure 4.6	Graph of Predicted vs. Actual Values for the Model	133
Figure 4.7	Perturbation Plot of the Vibration Model	134

Figure 4.8 3D Interaction Plot of Speed (Depth of Cut	Vibration Amplitude versus Feed and Cutting Kept Constant at the Central Value of 1.5 mm).	134
Figure 4.9 3D Interaction Plot of Cut (Cutting Speed K	Vibration Amplitude versus Feed and Depth of ept Constant at the Central Value of 125 m/min)	135
Figure 4.10 Screen Shot of Optim Minimum Vibration	num Solutions of the Numerical Optimization for Amplitude	137
Figure 4.11 Contour Plot of Opti Depth of Cut	mum Solutions for Combinations of Feed and	138
Figure 4.12 Overlay Plot Showir	g the Results of Graphical Optimization	139
Figure 4.13 Screen Shot of Sugg Amplitude for Mode	ested Conditions of Cut and Predicted Vibration I's Confirmatory Test from DOE	141
Figure 4.14 (a) Time Domain Plo (Cutting Speed 50 m Used for Confirmato	ot and (b) FFT Analysis for the Experimental Run /min, Feed 0.10 mm/rev and Depth of Cut 1.2 mm ory Test.	n) 142
Figure 4.15 Sample Calculation Stainless Steel Chip Feed 0.22 mm/rev ar	of Chip Serration Frequency Using SEM Image of Obtained at Cutting Speed 200 m/min, RPM 625, nd DOC 1.0 mm.	f 145
Figure 4.16 Perturbation Plot of	the Chip Serration Model	147
Figure 4.17 3D Response Surfac and Cutting Speed (1 1.5 mm).	e Plot of Chip Serration Frequency versus Feed Depth of Cut Kept Constant at the Central Value of	of 148
Figure 4.18 Plot of Predicted ver	sus Actual Values for Precision Determination	152
Figure 4.19 Perturbation Plot of	the Cutting Force Model	153
Figure 4.20 3D Interaction Plot of	of Cutting Force versus Cutting Speed and DOC.	154
Figure 4.21 3D Interaction Plot of	of Cutting Force versus Feed and Depth of Cut	154
Figure 4.22 Suggested Optimum	Solutions of the Numerical Optimization	156
Figure 4.23 Contour Plot of Opti Depth of Cut	mum Solutions for Combinations of Feed and	157
Figure 4.24 Overlay Plot Showir	ng the Results of Graphical Optimization	158
Figure 4.25 Suggested Condition for Model's Confirm	as of Cut and Predicted Cutting Force Amplitude natory Test	160
Figure 5.1 SEM Images of Chips	Obtained at Different Cutting Speeds (Feed and	

Depth of Cut Kept Constant at 1.6 mm/rev and 1.5 mm, respectively):

	(a) $Vc = 18.93$ m/min, (b) $Vc = 28.93$ m/min, (c) $Vc = 38.93$ m/min an (d) $Vc = 48.93$ m/min.	d 169
Figure 5.2	SEM Images of Two Chips Obtained at Different Cutting Speeds and Sample Calculations for Chip Serration Frequency Determination.	170
Figure 5.3	Vibration Amplitude and Chip Serration Frequency vs. Cutting Speed	171
Figure 5.4	Cutting Force and Chip Serration Frequency vs. Cutting Speed	171
Figure 5.5	Cutting Force and Vibration Amplitude vs. Cutting Speed	172
Figure 5.6	SEM Images of Chips Obtained at Different Cutting Speeds Near Vc = 68.93 m/min (Feed and Depth of Cut Kept Constant at 1.6 mm/rev and mm, respectively): (a) Vc = 58.93 m/min , (b) Vc = 68.93 m/min and (c = 78.93 m/min .	1.5) Vc 172
Figure 5.7	SEM Images of Chips Obtained at Different Cutting Speeds Near Vc = 118.93 m/min (Feed and Depth of Cut Kept Constant at 1.6 mm/rev an 1.5 mm, respectively): (a) Vc = 108.93 m/min, (b) Vc = 118.93 m/min (c) Vc = 128.93 m/min.	d and 173
Figure 5.8	Free Body Force Diagram of the Flexible Tool-Work-piece System	179
Figure 5.9	Cantilever Beam Model of the Tool Shank with Base Excitation	181
Figure 5.1	 0 Cantilever Beam Arrangement with Base Excitation and the Equivaler 1 DOF Lumped Body Model with Mass, Damper and Spring Setup. 	nt 181
Figure 5.1	1 Time Domain Output of Vibration Amplitude Decay Derived from Knocking Test of Tool Shank with TOH 120 mm.	184
Figure 6.1	Schematics of a Parallel and Non-Interacting General PID Controller (Dorf & Bishop, 1998).	194
Figure 1.2	Schematics of the PI Based Online Chatter Controller	198
Figure 1.3	Vibration Signals Obtained from Turning Under the Central Run Conditions. These Types of Readings were utilized for RMS Calculation for PI Controller Set Point Determination	on 199
Figure 1.4	Comparison of Resultant Vibration Amplitudes for the 15 DOE Runs	202
Figure 1.5	Percentage Vibration Reduction for the 15 DOE Runs	202
Figure 1.6	Frequency and Time Domain Plots for Run 6 (Cutting Speed 18.93 m/r Feed 0.16 mm/rev and DOC 1.50 mm) for: (a) Undamped Turning and Damped Turning.	nin, (b) 203

LIST OF ABBREVIATIONS

2FI	Two-factor interaction
3D	Three dimensional
V _c	Cutting speed
f	Feed rate
DOC	Depth of cut
ANOVA	Analysis of variance
DOE	Design of experiment
CCD	Central composite design
RSM	Response surface methodology
CNC	Computer numerical control
DAQ	Data acquisition
DF	Degree of freedom
F _c	Cutting force
f_c	Chip serration frequency
$\mathbf{f}_{\mathbf{n}}$	Natural frequency
FEA	Finite element analysis
FFT	Fast Fourier transforms
Hz	Hertz
mm	millimetre
Ν	Newton
SEM	Scanning electron microscope
SS	Sum of squares
MRR	Material removal rate

CHAPTER ONE INTRODUCTION

1.1 BACKGROUND

A major activity in most manufacturing processes is the removal of materials using tools to produce parts having required shape, dimensions and accuracy. Such subtractive manufacturing or removal processes are termed as machining and are essentially 'chip or swarf removing' processes. These processes represent the largest class of manufacturing activities in the industry. As, metals and their alloys represent the most common materials which are machined, the term 'metal cutting' is often used instead of machining (Trent & Wright, 2000).

Turning is the most common and basic machining process which has remained virtually unchanged since early 18th century (Trent & Wright, 2000). It is usually accomplished using machine tools known as lathes. Like most machining operations, turning is often plagued by chatter which accelerates tool wear, increases surface roughness, and reduces process predictability and productivity. Therefore, chatter is of serious concern in both research and industry.

Machine tool chatter is a type of intense self-excited vibration between the individual parts of a Machine-Tool-Fixture-Work (MTFW) system. The prevalent practice in chatter avoidance has been to reduce the cutting speed, which unfortunately lowers material removal rate and productivity.

Although, chatter has been extensively investigated since its first identification by Taylor (1907) over a 100 years ago, and several hypotheses and theories have been developed, the root cause of chatter and its mechanism of formation still remain controversial (Amin, 1982). This is because the phenomenon of chatter is very complex and there are many sources of vibration in the MTFW system (Amin & Patwari, 2011).

Most research works have focused on the basic theories and mechanics of mechanical vibration or the role of structural dynamics of the machine tool to understand chatter (Amin & Patwari, 2011). Yet others have viewed chatter from an analytical approach to the mechanics of machining and assessing machinability (Oxley & Young, 1989). However, on most occasions, chatter has remained elusive, inexplicable and unpredictable (Tarng, Young & Lee, 1994).

Among the established theories of chatter, the most widely used one is the Regenerative Chatter theory (Tobias, 1965). The theory posits that vibration marks on the work-piece, left from previous cuts in the form of surface waviness, are responsible for generating chatter in the subsequent cuts (Wiercigroch & Budak, 2001). However, the regenerative theory of chatter fails to explain the incidence of chatter in helical turning of a ground work-piece having no chatter marks from the previous pass (Amin & Patwari, 2011). Therefore, a more generalized and effective theory and model for chatter, especially in metal turning operations, is required.

Amin (1982), and Amin and Patwari (2011) have explained chatter as a resonance phenomenon which arises in the system when the chip serration frequency coincides with the prominent natural frequencies (or higher harmonics) of the MTFW system. They investigated in detail the instability of chip formation in machining and observed the formation of primary and secondary 'serration or saw teeth' on the resultant chips. This led to the insight that the root cause of chatter in end milling was a resonance phenomenon (Amin, 1982; Patwari, Amin & Faris, 2010). Building on this conclusion, turning, which is also a basic metal cutting process, is expected to have a similar formative mechanism of chatter. Nevertheless, the elastic system of

turning is different from that of a vertical milling machine and the components of the system have different configurations and natural frequencies. For instance, milling is an interrupted cutting process whereas turning is a continuous process. In addition, there is as yet no consensus among the different researchers on the main cause of chatter in turning and how best to model it. Hence, it is essential to study in detail the system dynamics and the cutting parameters related to chip formation instabilities and the interaction of the chip serration frequencies with the system's natural frequencies. This would lead to a correct understanding of the mechanism of chatter in turning, which is the main focus of this research.

Chatter control is another important area in manufacturing industry where its detrimental effects on process economics and its unpredictability have spurred the development of many chatter control methods. However, most, if not all, of these existent chatter control methods are expensive or difficult to implement. Thus, this research also focuses on the development of a simple, yet robust and economical, online chatter control method.

1.2 PROBLEM STATEMENT

Although many research works have been conducted on chatter and its modelling, an extensive literature search seems to indicate the absence of a comprehensive chatter theory for turning with reliable predictions of the onset of chatter under varying conditions of cut. Existing theories and hypotheses are mostly contradictory in nature and sometimes do not agree with experimental observations. The prevalent Regenerative Theory of Chatter by Tobias (1965) fails to explain chatter during helical thread cutting or turning of highly polished metals. Other works are purely experimental in nature, trying to understand the phenomenon of chatter from empirical

observations and devising ways to eliminate it (Amin & Patwari, 2011; Amin, 1982). Yet others, for instance Patwari (2010), addressed the phenomenon of chatter for end milling operations only. Thus there are few, if any, contemporary research work effectively explaining and modelling chatter, especially for turning of stainless steel. Therefore, it is of paramount importance to develop an effective model of chatter and to validate it using experimental data for different conditions of cut. The proposed model of chatter in the current research work is intended to be formulated based on chip serration, dynamic characteristics of the MTFW system, cutting force, primary cutting parameters and resultant machining vibrations; all of which have not been taken into consideration, in a comprehensive manner, in previous research works. The intended model will be developed based on an in-depth understanding of chatter formation mechanism derived from experimental observations of the chip serration with system dynamics via mode coupling as the primary player in the generation of chatter.

In addition, a viable and effective chatter control strategy in turning of stainless steel is needed. Most existing chatter damping methods are costly, complicated or difficult to implement. Yet others are based solely on heuristics, such as variations in spindle speed or trial and error methods. Thus, coincident with model development, the current research work intends to develop an online chatter control strategy and test its ability to reduce vibration amplitude during turning of stainless steel at different conditions of cut. The technique proposed for such chatter control is the application of magnetic fields from electromagnet controlled via a closed-loop computerised control system.

1.3 SIGNIFICANCE AND BENEFITS OF THE RESEARCH

The developed mathematical models of chatter and the online damping technique will be very useful for metal cutting industries, especially the automotive and structural member fabrication industries which use steel very widely. The theory will also help researchers gain a clearer understanding of chatter as well as enable them to standardize and optimise chatter free steel turning operations for industrial applications. The model and theory will pave the way for newer avenues of research in this field. Upon completion, the current research will lead to the following specific benefits:

- 1. Better in-depth and quantitative understanding of the mechanics of chatter formation in turning operations involving AISI 304 stainless steel.
- Accurate prediction of the incidence of chatter which can be implemented in research work or industrial processes involving turning of stainless steel, a very common and important work material in aerospace, automotive, structural part or component manufacturing and food processing industries.
- 3. Development of a novel online chatter control system based on electromagnetic damping technique.
- 4. The developed models and implementation of the chatter control system in the manufacturing industry could lead to the following benefits:
 - a. Higher dimensional accuracy and improved surface finish of machined parts.
 - b. Greater material removal rate and production efficiency.
 - c. Increased process predictability and reliability which could facilitate automation.

- d. Significantly longer tool life and better machine tool performance which would lead to better process economics.
- e. Avoidance of catastrophic tool or machine tool failure, hence increase in process safety.
- f. Reduction of reworks and wastages.
- g. Cancelation of loud high pitched noise associated with chatter during machining operations.
- h. Elimination of the need for using cutting fluid making turning of stainless steel more environmentally friendly.

1.4 RESEARCH PHILOSOPHY

This research study is designed based on the historical roots of the physical phenomenon of chatter formation in machine tools. Different hypotheses, employing both theoretical and empirical approaches, were evaluated in depth based on their merits and limitations. The philosophical assumption of this research is made based on the experimental findings of previous and current research on: the discreet nature of chip formation, vibration spectral analysis and cutting force during turning. Past research works have used quantitative, qualitative and mixed-method approaches to explain chatter formation (Patwari, 2010).

The current research employed a positivist philosophical approach to address the research questions. This philosophy dictates that vital and relevant information is obtained by adopting a precise, programmed approach when gathering data. This mode of thinking preaches an objective approach to understanding reality where emphasis is put on quantitative precision and the collection of relevant factual data in order to build knowledge and obtain a closer estimation of reality without any